intermediate cylindrical portion 32 and a shoulder portion 34. The intermediate portion and split ring portions outer diameters are uniform. The wear sleeve is inserted into the bit holder's stepped bore aperture by the use of a hammer. The split ring portion 30 is radially compressed by the smaller diameter opposite end portion 30 as the sleeve is hammered into position in the bit holder. The split ring portion forms adequate frictional contact with the opposite end portion of the aperture. The wear sleeve friction fit can be easily removed manually in the field.

Please delete the entire paragraph beginning on page 5, line 28, through page 6, line 4, and replace it with the following paragraph:

Figure 2a discloses in more detail the wear sleeve 14, the bit holder 12 and the support block 10. The bit holder 12 is connected to the support block 10 by a bolt 18. The support block has a bore for receiving the bolt 18. A washer 20 is placed on the bolt head prior to inserting the bolt into a bore. The bolt is threaded into a threaded portion of the bore in the bit holder. The bolt is then tightened to wedge the bit holder into position on the support block.

Please delete the entire paragraph beginning on page 7, line 3, through line 23, and replace it with the following paragraph:

In one example of this embodiment, the forward end portion of the step bore diameter (A) is 1.185" and the opposite end portion of the step bore 28 diameter (B) is 1.166". The outside diameter (C) of the wear sleeve is 1.181" and has an inner diameter of .783". The split ring portion of the wear sleeve upon insertion into the bit holder bore is radially compressed and squeezed into position. The slot 31 is approximately .12" inches in width to enable the split ring portion to be squeezed into the smaller diameter portion 28 of the step bore. The slot extends for less than half the length of the wear sleeve body. The split spring portion is made from a spring like resilient material

that upon insertion into the stepped bore becomes biased and exerts a radial force component against the bore surface. The wear sleeve can be constructed from 4140 Steel. A resultant axial frictional force component exists between the cooperating contact surfaces of the split ring wear sleeve and smaller diameter portion the stepped bore. This frictional fit holds the wear sleeve in position against axial pulling forces on the cutting tool.

Please delete the entire paragraph beginning on page 8, line 33, through page 9, line 15, and replace it with the following paragraph:

Figure 2 shows the front view of the first embodiment in which the support block groove 19 and T-shaped Key 44 are illustrated. The bit holder 12 rests on top of the support block on symmetric top surfaces 46 adjacent to the centrally located groove 19. The top surfaces 46 of the support block are oriented at an angle (beta) with respect to the horizontal. In the prior art these surfaces are angled at approximately 10 degrees to the horizontal. The present design includes an angle of at least 15 degrees. In one contemplated embodiment the top surfaces are angled at about 15 degrees. The bit holder has a surface that forms a complimentary angle with the top surface of the support block so that the bit holder makes uninterrupted contact with surface 46. This angle of inclination prevents back and forth movement along Z-axis. This inhibition of movement of the bit holder away from the Z-axis accordingly limits rotation about the Y axis. This reduction in yaw about the Y axis reduces the amount of wear between the bit holder and support block.

Please delete the entire paragraph beginning on page 9, line 35, through page 10, line 10, and replace it with the following paragraph:

In figure 2 a bore hole 17 is illustrated that traverses the length of the bit holder shank from an opening on the front face to an opening on the rearward face. The portion of the bit holder adjacent to the

rearward face is threaded for receiving bolt 18. The forward portion of the bore is for the purpose of preferentially weakening the block by reducing the cross sectional area along a plane of the bit holder. When abnormally high loads are applied to the cutting tool bit holders the bit holder will break along this preferentially weakened portion of the bit holder and prevent the support block from being ripped off the drum.

Please delete the entire paragraph beginning on page 9, line 16, through line 34, and replace it with the following paragraph:

In addition to the angle of inclination of the top faces 46 of the support block and correspond bit holder surfaces. The bit holder bore 24 is positioned more aft from the central axis N-N as seen in Figure 2a than prior art bit holder bores. In figure 2a, 75% of the bit holder 12 bore is positioned aft of the central vertical axis N—N. The bit holder bore location results in the cutting tool 16 tip location being positioned more towards the aft and closer to the central axis N-N. The closer that the extreme tip of the cutting tool is to the support block central axis N-N the shorter the effective moment arm about the central axis. Hence the torques applied to the bit holder are limited and hence the resulting wear caused by movement of the bit holder against the support block is reduced. In combination the further aft location of the cutting tool and the angled top faces of the support block substantially reduce the torque applied to the cutting tool and the resulting yaw. The reduced yaw of the bit holder results in extended life of the bit holder and support block.

IN THE ABSTRACT:

Please substitute the following Abstract for the original Abstract: